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DESCRIPTION**POLARIZER, OPTICAL FILM AND IMAGE DISPLAY****Technical Field**

5 [0001]

The present invention relates to a polarizer. This invention also relates to a polarizing plate and an optical film using the polarizer concerned. Furthermore, this invention relates to an image display, such as a liquid crystal display, an organic electroluminescence display, a CRT and a PDP using the polarizing plate and the optical film concerned.

Background Art

[0002]

15 Liquid crystal display are rapidly developing in market, such as in clocks and watches, cellular phones, PDAs, notebook-sized personal computers, and monitor for personal computers, DVD players, TVs, etc. In the liquid crystal display, visualization is realized based on a variation of polarization state by switching of a liquid crystal, where polarizers are used based on a display principle thereof. Particularly, usage for TV etc. increasingly requires display with high luminance and high contrast, polarizers having higher brightness (high transmittance) and higher contrast (high polarization degree) are being developed and introduced.

25 [0003]

As polarizers, for example, since it has a high transmittance and a high polarization degree, polyvinyl alcohols having a structure in which iodine is absorbed and then stretched, that is, iodine based polarizers are widely used (for

example, Japanese Patent Laid-Open No.2001-296427). However, since the iodine based polarizers have relatively low polarization degrees in short wavelength side, they have problems in hue, such as blue omission in black viewing, and yellowing in white viewing, in short wavelength side.

[0004]

Iodine based polarizers may easily give unevenness in a process of iodine absorption. Accordingly, there has been a problem that the unevenness is detected as unevenness in transmittance particularly in the case of black viewing, causing to decrease of visibility. For example, as methods for solving the problems, several methods have been proposed that an amount of absorption of iodine absorbed to the iodine based polarizer is increased and thereby a transmittance in the case of black viewing is set not higher than sensing limitations of human eyes, and that stretching processes generating little unevenness itself are adopted. However, the former method has a problem that it decreases a transmittance in the case of white viewing, while decreasing a transmittance of black viewing, and as a result darkens the display itself. And also, the latter method has a problem that it requires replacing a process itself, worsening productivity.

[0005]

It is also noted that an iodine based polarizer is low in thermal durability. To be concrete, there has been a problem that a hue changes at a high temperature.

Disclosure of Invention

[0006]

This invention aims at providing an iodine based polarizer

having a high polarization degree even on the short wavelength and excels in durability.

[0007]

Moreover, this invention aims at providing an iodine based polarizer having a high transmittance and a high polarization degree, and being able to control unevenness of the transmittance in the case of black viewing, and excels in durability.

[0008]

Besides, this invention aims at providing a polarizing plate and an optical film using the polarizer concerned. Furthermore, this invention aims at providing an image display using the polarizer, the polarizing plate, and the optical film concerned.

[0009]

As a result of examination wholeheartedly performed by the present inventors that the above-mentioned subject should be solved, it was found out that the above-mentioned purpose might be attained using polarizers shown below, leading to completion of this invention.

[0010]

That is, this invention relates to a polarizer comprising a film having a structure having a minute domain dispersed in a matrix formed of a translucent water-soluble resin including an iodine light absorbing material and a divalent metal.

[0011]

The minute domain of the above-mentioned polarizer is preferably formed by an oriented birefringent material. The above-mentioned birefringent material preferably shows liquid crystallinity at least in orientation processing step.

[0012]

The above-mentioned polarizer of this invention has an iodine based polarizer formed by a translucent water-soluble resin and an iodine based light absorbing material as a matrix, and has dispersed minute domains in the above-mentioned matrix. Minute domains are preferably formed by oriented materials having birefringence, and particularly minute domains are formed preferably with materials showing liquid crystallinity. Thus, in addition to function of absorption dichroism by iodine based light absorbing materials, characteristics of having function of scattering anisotropy improve polarization performance according to synergistic effect of the two functions, and as a result a polarizer having both of transmittance and polarization degree, and excellent visibility may be provided.

[0013]

Iodine based light absorbing material means chemical species comprising iodine and absorbs visible light, and it is thought that, in general, they are formed by interaction between translucent water-soluble resins (particularly polyvinyl alcohol based resins) and poly iodine ions (I_3^- , I_5^- , etc.). An iodine based light absorbing material is also called an iodine complex. It is thought that poly iodine ions are generated from iodine and iodide ions.

[0014]

Scattering performance of anisotropic scattering originates in refractive index difference between matrixes and minute domains. For example, if materials forming minute domains are liquid crystalline materials, since they have higher wavelength dispersion of Δn compared with translucent water-soluble resins as a matrix, a refractive index difference in

scattering axis becomes larger in shorter wavelength side, and, as a result, it provides more amounts of scattering in shorter wavelength. Accordingly, an improving effect of large polarization performance is realized in shorter wavelengths, compensating a relative low level of polarization performance of an iodine based polarizer in a side of shorter wavelength, and thus a polarizer having high polarization and neutral hue may be realized.

[0015]

Besides, an iodine based polarizer of the invention contains a divalent metal in the matrix. As divalent metals, it is preferable to contain zinc and/or nickel. By containing a divalent metal therein, a change in hue can be suppressed and thermal durability can be improved. A divalent metal salt is used in order to obtain a divalent metal contained in the matrix and the divalent metal is usually contained as a divalent metal ion in the matrix. It is disclosed in Japanese Patent Application Laid-open Publication No.54-16575, Japanese Patent Application Laid-open Publication No.2-34001, Japanese Patent Application Laid-open No.2000-35512 and the like that thermal durability can be improved by dispersing a divalent metal into a water-soluble resin such as polyvinyl alcohol.

[0016]

In the above-mentioned polarizer, it is preferable that the minute domains have a birefringence of 0.02 or more. In materials used for minute domains, in the view point of gaining larger anisotropic scattering function, materials having the above-mentioned birefringence may be preferably used.

[0017]

In the above-mentioned polarizer, in a refractive index

difference between the birefringent material forming the minute domains and the translucent water-soluble resin in each optical axis direction, a refractive index difference (Δn^1) in direction of axis showing a maximum is 0.03 or more, and a refractive index difference (Δn^2) between the Δn^1 direction and a direction of axes of two directions perpendicular to the Δn^1 direction is 50% or less of the Δn^1 .

[0018]

Control of the above-mentioned refractive index difference (Δn^1) and (Δn^2) in each optical axis direction into the above-mentioned range may provide a scattering anisotropic film having function being able to selectively scatter only linearly polarized light in the Δn^1 direction, as is submitted in U.S. Pat. No. 2123902 specification. That is, on one hand, having a large refractive index difference in the Δn^1 direction, it may scatter linearly polarized light, and on the other hand, having a small refractive index difference in the Δn^2 direction, and it may transmit linearly polarized light. Moreover, refractive index differences (Δn^2) in the directions of axes of two directions perpendicular to the Δn^1 direction are preferably equal.

[0019]

In order to obtain high scattering anisotropy, a refractive index difference (Δn^1) in a Δn^1 direction is set 0.03 or more, preferably 0.05 or more, and still preferably 0.10 or more. A refractive index difference (Δn^2) in two directions perpendicular to the Δn^1 direction is 50% or less of the above-mentioned Δn^1 , and preferably 30% or less.

[0020]

In iodine based light absorbing material in the above-mentioned polarizer, an absorption axis of the material

concerned preferably is orientated in the Δn^1 direction.

[0021]

The iodine based light absorbing material in a matrix is orientated so that an absorption axis of the material may become parallel to the above-mentioned Δn^1 direction, and thereby linearly polarized light in the Δn^1 direction as a scattering polarizing direction may be selectively absorbed. As a result, on one hand, a linearly polarized light component of incident light in a Δn^2 direction is not scattered or hardly absorbed by the iodine light absorbing material as in conventional iodine based polarizers without anisotropic scattering performance. On the other hand, a linearly polarized light component in the Δn^1 direction is scattered, and is absorbed by the iodine based light absorbing material. Usually, absorption is determined by an absorption coefficient and a thickness. In such a case, scattering of light greatly lengthens an optical path length compared with a case where scattering is not given. As a result, polarized component in the Δn^1 direction is more absorbed as compared with a case in conventional iodine based polarizers. That is, higher polarization degrees may be attained with same transmittances.

[0022]

Descriptions for ideal models will, hereinafter, be given. Two main transmittances usually used for linear polarizer (a first main transmittance k_1 (a maximum transmission direction = linearly polarized light transmittance in a Δn^2 direction), a second main transmittance k_2 (a minimum transmission direction = linearly polarized light transmittance in a Δn^1 direction)) are, hereinafter, used to give discussion.

[0023]

In commercially available iodine based polarizers, when iodine based light absorbing materials are oriented in one direction, a parallel transmittance and a polarization degree may be represented as follows, respectively:

$$\begin{aligned} \text{parallel transmittance} &= 0.5 \times ((k_1)^2 + (k_2)^2) \text{ and} \\ \text{polarization degree} &= (k_1 - k_2) / (k_1 + k_2). \end{aligned}$$

[0024]

On the other hand, when it is assumed that, in a polarizer of this invention, a polarized light in a Δn^1 direction is scattered and an average optical path length is increased by a factor of α (> 1), and depolarization by scattering may be ignored, main transmittances in this case may be represented as k_1 and $k_2' = 10^x$ (where, x is $\alpha \log k_2$), respectively

[0025]

That is, a parallel transmittance in this case and the polarization degree are represented as follows:

$$\begin{aligned} \text{parallel transmittance} &= 0.5 \times ((k_1)^2 + (k_2')^2) \text{ and} \\ \text{polarization degree} &= ((k_1 - k_2') / (k_1 + k_2')). \end{aligned}$$

[0026]

When a polarizer of this invention is prepared by a same condition (an amount of dyeing and production procedure are same) as in commercially available iodine based polarizers (parallel transmittance 0.385, polarization degree 0.965: $k_1 = 0.877$, $k_2 = 0.016$), on calculation, when α is 2 times, k_2 becomes small reaching 0.0003, and as result, a polarization degree improves up to 0.999, while a parallel transmittance is maintained as 0.385. The above-mentioned result is on calculation, and function may decrease a little by effect of depolarization caused by scattering, surface reflection, backscattering, etc. As the above-mentioned equations show,

higher value α may give better results and higher dichroic ratio of the iodine based light absorbing material may provide higher function. In order to obtain higher value α , a highest possible scattering anisotropy function may be realized and polarized light in a Δn^1 direction may just be selectively and strongly scattered. Besides, less backscattering is preferable, and a ratio of backscattering strength to incident light strength is preferably 30% or less, and more preferably 20% or less.

[0027]

As the above-mentioned polarizers, films manufactured by stretching may suitably be used.

[0028]

In the above-mentioned polarizer, minute domains preferably have a length in a Δn^2 direction of 0.05 to 500 μm .

[0029]

In order to scatter strongly linearly polarized light having a plane of vibration in a Δn^1 direction in wavelengths of visible light band, dispersed minute domains have a length controlled to 0.05 to 500 μm in a Δn^2 direction, and preferably controlled to 0.5 to 100 μm . When the length in the Δn^2 direction of the minute domains is too short compared with wavelengths, scattering may not fully provided. On the other hand, when the length in the Δn^2 direction of the minute domains is too long, there is a possibility that a problem of decrease in film strength or of liquid crystalline material forming minute domains not fully oriented in the minute domains may arise.

[0030]

In the above-mentioned polarizer, iodine light absorbing materials having an absorption band at least in a wavelength range of 400 to 700nm may be used.

[0031]

In the above-mentioned polarizers, a transmittance to a linearly polarized light in a transmission direction is 80% or more, a haze value is 5% or less, and a haze value to a linearly polarized light in an absorption direction is 30% or more.

[0032]

An iodine polarizer of this invention having the above-mentioned transmittance and haze value has a high transmittance and excellent visibility for linearly polarized light in a transmission direction, and has strong optical diffusibility for linearly polarized light in an absorption direction. Therefore, without sacrificing other optical properties and using a simple method, it may demonstrate a high transmittance and a high polarization degree, and may control unevenness of the transmittance in the case of black viewing.

[0033]

As a polarizer of this invention, a polarizer is preferable that has as high as possible transmittance to linearly polarized light in a transmission direction, that is, linearly polarized light in a direction perpendicular to a direction of maximal absorption of the above-mentioned iodine based light absorbing material, and that has 80% or more of light transmittance when an optical intensity of incident linearly polarized light is set to 100. The light transmittance is preferably 85% or more, and still preferably 88% or more. Here, a light transmittance is equivalent to a value Y calculated from a spectral transmittance in 380 nm to 780 nm measured using a spectrophotometer with an integrating sphere based on CIE 1931 XYZ standard colorimetric system. In addition, since about 8% to 10% is reflected by an air interface on a front surface and rear surface of

a polarizer, an ideal limit is a value in which a part for this surface reflection is deducted from 100%.

[0034]

It is desirable that a polarizer does not scatter linearly polarized light in a transmission direction in the view point of obtaining clear visibility of a display image. Accordingly, the polarizer preferably has 5% or less of haze value to the linearly polarized light in the transmission direction, more preferably 3% or less, and still more preferably 1% or less. On the other hand, in the view point of covering unevenness by a local transmittance variation by scattering, a polarizer desirably scatters strongly linearly polarized light in a absorption direction, that is, linearly polarized light in a direction for a maximal absorption of the above-mentioned iodine based light absorbing material. Accordingly, a haze value to the linearly polarized light in the absorption direction is preferably 30% or more, more preferably 40% or more, and still more preferably 50% or more. In addition, the haze value here is measured based on JIS K 7136 (how to obtain a haze of plastics-transparent material).

[0035]

The above-mentioned optical properties are obtained by compounding a function of scattering anisotropy with a function of an absorption dichroism of the polarizer. As is indicated in U.S. Pat. No. 2123902 specification, Japanese Patent Laid-Open No.9-274108, and Japanese Patent Laid-Open No.9-297204, same characteristics may probably be attained also in a way that a scattering anisotropic film having a function to selectively scatter only linearly polarized light, and a dichroism absorption type polarizer are superimposed in an axial arrangement so that an axis providing a greatest scattering and an axis providing a

greatest absorption may be parallel to each other. These methods, however, require necessity for separate formation of a scattering anisotropic film, have a problem of precision in axial joint in case of superposition, and furthermore, a simple
5 superposition method does not provide increase in effect of the above-mentioned optical path length of the polarized light absorbed as is expected, and as a result, the method cannot easily attain a high transmission and a high polarization degree.
[0036]

10 Besides, this invention relates to a polarizing plate which having a transparent protection layer at least on one side of the above-mentioned polarizer.
[0037]

Moreover, this invention relates to an optical film
15 characterized by being laminated with at least one of the above-mentioned polarizer and the above-mentioned polarizing plate.
[0038]

Furthermore, this invention relates to an image display
20 characterized by using the above-mentioned polarizer, the above-mentioned polarizing plate, or the above-mentioned optical film.

Brief Description of Drawing

25 [0039]

Fig. 1 is conceptual view showing an example of a polarizer of this invention;

Best Mode for Carrying Out the Invention

30 [0041]

A polarizer of this invention will, hereinafter, be described referring to drawings. Fig. 1 is a conceptual view of a polarizer of this invention, and the polarizer has a structure where a film is formed with a translucent water-soluble resin 1 including an iodine based light absorbing material 2a and a divalent metal, which is not shown in FIG., and minute domains 3 are dispersed in the film concerned as a matrix.

[0042]

Fig. 1 shows an example of a case where the iodine based light absorbing material 2a is oriented in a direction of axis (Δn^1 direction) in which a refractive index difference between the minute domain 3 and the translucent water-soluble resin 1 shows a maximal value. In minute domain 3, polarized components in the Δn^1 direction are scattered. In Fig. 1, the Δn^1 direction in one direction in a film plane is an absorption axis. In the film plane, a Δn^2 direction perpendicular to the Δn^1 direction serves as a transmission axis. Another Δn^2 direction perpendicular to the Δn^1 direction is a thickness direction.

[0043]

As translucent water-soluble resins 1, resins having translucency in a visible light band and dispersing and absorbing the iodine based light absorbing materials may be used without particular limitation. For example, polyvinyl alcohols or derivatives thereof conventionally used for polarizers may be mentioned. As derivatives of polyvinyl alcohol, polyvinyl formals, polyvinyl acetals, etc. may be mentioned, and in addition derivatives modified with olefins, such as ethylene and propylene, and unsaturated carboxylic acids, such as acrylic acid, methacrylic acid, and crotonic acid, alkyl esters of unsaturated carboxylic acids, acrylamides etc. may be mentioned. Besides,

as translucent water-soluble resin 1, for example, polyvinyl pyrrolidone based resins, amylose based resins, etc. may be mentioned. The above-mentioned translucent water-soluble resin may be of resins having isotropy not easily generating orientation birefringence caused by molding deformation etc., and of resins having anisotropy easily generating orientation birefringence.

[0044]

A divalent metal 2b is usually contained as a divalent metal ion. No limitation is imposed on a kind of a divalent metal 2b, but, for example, zinc, nickel and the like are preferably used because of good thermal durability. Divalent metals can be used either alone or in combination of two or more kinds. For impregnation of a divalent metal, an aqueous solution of a divalent metal such as a chloride, a sulfate, a nitrate or the like are generally used.

[0045]

In materials forming minute domains 3, it is not limited whether the material has birefringence or isotropy, but materials having birefringence is particularly preferable. Moreover, as materials having birefringence, materials (henceforth, referred to as liquid crystalline material) showing liquid crystallinity at least at the time of orientation treatment may preferably used. That is, the liquid crystalline material may show or may lose liquid crystallinity in the formed minute domain 3, as long as it shows liquid crystallinity at the orientation treatment time.

[0046]

As materials forming minute domains 3, materials having birefringences (liquid crystalline materials) may be any of materials showing nematic liquid crystallinity, smectic liquid crystallinity, and cholesteric liquid crystallinity, or of materials

showing lyotropic liquid crystallinity. Moreover, materials having birefringence may be of liquid crystalline thermoplastic resins, and may be formed by polymerization of liquid crystalline monomers. When the liquid crystalline material is of liquid crystalline thermoplastic resins, in the view point of heat-resistance of structures finally obtained, resins with high glass transition temperatures may be preferable. Furthermore, it is preferable to use materials showing glass state at least at room temperatures. Usually, a liquid crystalline thermoplastic resin is oriented by heating, subsequently cooled to be fixed, and forms minute domains while liquid crystallinity are maintained. Although liquid crystalline monomers after orienting can form minute domains in the state of fixed by polymerization, cross-linking, etc., some of the formed minute domains may lose liquid crystallinity.

[0047]

As the above-mentioned liquid crystalline thermoplastic resins, polymers having various skeletons of principal chain types, side chain types, or compounded types thereof may be used without particular limitation. As principal chain type liquid crystal polymers, polymers, such as condensed polymers having structures where mesogen groups including aromatic units etc. are combined, for example, polyester based, polyamide based, polycarbonate based, and polyester imide based polymers, may be mentioned. As the above-mentioned aromatic units used as mesogen groups, phenyl based, biphenyl based, and naphthalene based units may be mentioned, and the aromatic units may have substituents, such as cyano groups, alkyl groups, alkoxy groups, and halogen groups.

[0048]

As side chain type liquid crystal polymers, polymers having principal chain of, such as polyacrylate based, polymethacrylate based, poly-alpha-halo acrylate based, poly-alpha-halo cyano acrylate based, polyacrylamide based, polysiloxane based, and poly malonate based principal chain as a skeleton, and having mesogen groups including cyclic units etc. in side chains may be mentioned. As the above-mentioned cyclic units used as mesogen groups, biphenyl based, phenyl benzoate based, phenylcyclohexane based, azoxybenzene based, azomethine based, azobenzene based, phenyl pyrimidine based, diphenyl acetylene based, diphenyl benzoate based, bicyclo hexane based, cyclohexylbenzene based, terphenyl based units, etc. may be mentioned. Terminal groups of these cyclic units may have substituents, such as cyano group, alkyl group, alkenyl group, alkoxy group, halogen group, haloalkyl group, haloalkoxy group, and haloalkenyl group. Groups having halogen groups may be used for phenyl groups of mesogen groups.

[0049]

Besides, any mesogen groups of the liquid crystal polymer may be bonded via a spacer part giving flexibility. As spacer parts, polymethylene chain, polyoxymethylene chain, etc. may be mentioned. A number of repetitions of structural units forming the spacer parts is suitably determined by chemical structure of mesogen parts, and the number of repeating units of polymethylene chain is 0 to 20, preferably 2 to 12, and the number of repeating units of polyoxymethylene chain is 0 to 10, and preferably 1 to 3.

[0050]

The above-mentioned liquid crystalline thermoplastic resins preferably have glass transition temperatures of 50°C or

more, and more preferably 80°C or more. Furthermore they have approximately 2,000 to 100,000 of weight average molecular weight.

[0051]

5 As liquid crystalline monomers, monomers having polymerizable functional groups, such as acryloyl groups and methacryloyl groups, at terminal groups, and further having mesogen groups and spacer parts including the above-mentioned cyclic units etc. may be mentioned. Crossed-linked structures
10 may be introduced using polymerizable functional groups having two or more acryloyl groups, methacryloyl groups, etc., and durability may also be improved.

[0052]

15 Materials forming minute domains 3 are not entirely limited to the above-mentioned liquid crystalline materials, and non-liquid crystalline resins may be used if they are different materials from the matrix materials. As the above-mentioned resins, polyvinyl alcohols and derivatives thereof, polyolefins, polyarylates, polymethacrylates, polyacrylamides, polyethylene
20 terephthalates, acrylic styrene copolymers, etc. may be mentioned. Moreover, particles without birefringence may be used as materials for forming the minute domains 3. As fine-particles concerned, resins, such as polyacrylates and acrylic styrene copolymers, may be mentioned. A size of the
25 fine-particles is not especially limited, and particle diameters of 0.05 to 500 μm may be used, and preferably 0.5 to 100 μm . Although it is preferable that materials for forming minute domains 3 is of the above-mentioned liquid crystalline materials, non-liquid crystalline materials may be mixed and used to the
30 above-mentioned liquid crystalline materials. Furthermore, as

materials for forming minute domains 3, non-liquid crystalline materials may also be independently used.

[0053]

5 In a polarizer of this invention, while producing a film in which a matrix is formed with a translucent water-soluble resin 1 including an iodine based light absorbing material 2a and a divalent metal 2b, minute domains 3 (for example, an oriented birefringent material formed with liquid crystalline materials) are dispersed in the matrix concerned. Moreover, the
10 above-mentioned refractive index difference (Δn^1) in a Δn^1 direction and a refractive index difference (Δn^2) in a Δn^2 direction are controlled to be in the above-mentioned range in the film.

[0054]

15 Manufacturing process of a polarizer of this invention is not especially limited, and for example, the polarizer of this invention may be obtained using following production processes:
(1) a process for manufacturing a mixed solution in which a material for forming minute domains is dispersed in a translucent water-soluble resin forming a matrix (description is,
20 hereinafter, to be provided, with reference to an example of representation, for a case where a liquid crystalline material is used as a material forming the minute domains. A case by a liquid crystalline material will apply to a case by other materials.);
25 (2) a process in which a film is formed with the mixed solution of the above-mentioned (1);
(3) a process in which the film obtained in the above-mentioned (2) is oriented (stretched)
(4) a process in which an iodine based light absorbing material is
30 dispersed (dyed) in the translucent water-soluble resin forming

the above-mentioned matrix; and

(5) a process in which a divalent metal is dispersing (impregnating) into the translucent water-soluble resin forming the above-mentioned matrix. In addition, an order of the processes (1) to (5) may suitably be determined.

[0055]

In the above-mentioned process (1), a mixed solution is firstly prepared in which a liquid crystalline material forming minute domains is dispersed in a translucent water-soluble resin forming a matrix. A method for preparing the mixed solution concerned is not especially limited, and a method may be mentioned of utilizing a phase separation phenomenon between the above-mentioned matrix component (a translucent water-soluble resin) and a liquid crystalline material. For example, a method may be mentioned in which a material having poor compatibility between the matrix component as a liquid crystalline material is selected, a solution of the material forming the liquid crystalline material is dispersed using dispersing agents, such as a surface active agent, in a water solution of the matrix component. In preparation of the above-mentioned mixed solution, some of combinations of the translucent material forming the matrix, and the liquid crystal material forming minute domains do not require a dispersing agent. An amount used of the liquid crystalline material dispersed in the matrix is not especially limited, and a liquid crystalline material is 0.01 to 100 parts by weight to a translucent water-soluble resin 100 parts by weight, and preferably it is 0.1 to 10 parts by weight. The liquid crystalline material is used in a state dissolved or not dissolved in a solvent. Examples of solvents, for example, include: water, toluene,

xylene, hexane cyclohexane, dichloromethane, trichloromethane, dichloroethane, trichloroethane, tetrachloroethane, trichloroethylene, methyl ethyl ketone, methylisobutylketone, cyclohexanone, cyclopentanone, tetrahydrofuran, ethyl acetate, etc. Solvents for the matrix components and solvents for the liquid crystalline materials may be of same, or may be of different solvents.

[0056]

In the above-mentioned process (2), in order to reduce foaming in a drying process after a film formation, it is desirable that solvents for dissolving the liquid crystalline material forming a minute domains is not used in preparation of the mixed solution in the process (1). When solvents are not used, for example, a method may be mentioned in which a liquid crystalline material is directly added to an aqueous solution of a translucency material forming a matrix, and then is heated above a liquid crystal temperature range in order to disperse the liquid crystalline material uniformly in a smaller state.

[0057]

In addition, a solution of a matrix component, a solution of a liquid crystalline material, or a mixed solution may include various kinds of additives, such as dispersing agents, surface active agents, ultraviolet absorption agents, flame retardants, antioxidants, plasticizers, mold lubricants, other lubricants, and colorants in a range not disturbing an object of this invention.

[0058]

In the process (2) for obtaining a film of the above-mentioned mixed solution, the above-mentioned mixed solution is heated and dried to remove solvents, and thus a film with minute domains dispersed in the matrix is produced. As

methods for formation of the film, various kinds of methods, such as casting methods, extrusion methods, injection molding methods, roll molding methods, and flow casting molding methods, may be adopted. In film molding, a size of minute domains in the film is controlled to be in a range of 0.05 to 500 μm in a Δn^2 direction. Sizes and dispersibility of the minute domains may be controlled, by adjusting a viscosity of the mixed solution, selection and combination of the solvent of the mixed solution, dispersant, and thermal processes (cooling rate) of the mixed solvent and a rate of drying. For example, a mixed solution of a translucent water-soluble resin that has a high viscosity and generates high shearing force and that forms a matrix, and a liquid crystalline material forming minute domains is dispersed by agitators, such as a homogeneous mixer, being heated at a temperature in no less than a range of a liquid crystal temperature, and thereby minute domains may be dispersed in a smaller state.

[0059]

The process (3) giving orientation to the above-mentioned film may be performed by stretching the film. In stretching, uniaxial stretching, biaxial stretching, diagonal stretching are exemplified, but uniaxial stretching is usually performed. Any of dries type stretching in air and wet type stretching in an aqueous system bath may be adopted as the stretching method. When adopting a wet type stretching, an aqueous system bath may include suitable additives (boron compounds, such as boric acid; iodide of alkali metal, etc.) A stretching ratio is not especially limited, and in usual a ratio of approximately 2 to 10 times is preferably adopted.

[0060]

This stretching may orient the iodine based light absorbing material in a direction of stretching axis. Moreover, the liquid crystalline material forming a birefringent material is oriented in the stretching direction in minute domains by the above-mentioned stretching, and as a result birefringence is demonstrated.

[0061]

It is desirable the minute domains may be deformed according to stretching. When minute domains are of non-liquid crystalline materials, approximate temperatures of glass transition temperatures of the resins are desirably selected as stretching temperatures, and when the minute domains are of liquid crystalline materials, temperatures making the liquid crystalline materials exist in a liquid crystal state such as nematic phase or smectic phase or an isotropic phase state, are desirably selected as stretching temperatures. When inadequate orientation is given by stretching process, processes, such as heating orientation treatment, may separately be added.

[0062]

In addition to the above-mentioned stretching, function of external fields, such as electric field and magnetic field, may be used for orientation of the liquid crystalline material. Moreover, liquid crystalline materials mixed with light reactive substances, such as azobenzene, and liquid crystalline materials having light reactive groups, such as a cinnamoyl group, introduced thereto are used, and thereby these materials may be oriented by orientation processing with light irradiation etc. Furthermore, a stretching processing and the above-mentioned orientation processing may also be used in combination. When the liquid crystalline material is of liquid crystalline thermoplastic resins,

it is oriented at the time of stretching, cooled at room temperatures, and thereby orientation is fixed and stabilized. Since target optical property will be demonstrated if orientation is carried out, the liquid crystalline monomer may not necessarily be in a cured state. However, in liquid crystalline monomers having low isotropic transition temperatures, a few temperature rise provides an isotropic state. In such a case, since anisotropic scattering may not be demonstrated but conversely polarized light performance deteriorates, the liquid crystalline monomers are preferably cured. Besides, many of liquid crystalline monomers will be crystallized when left at room temperatures, and then they will demonstrate anisotropic scattering and polarized light performance conversely deteriorate, the liquid crystalline monomers are preferably cured. In the view point of these phenomena, in order to make orientation state stably exist under any kind of conditions, liquid crystalline monomers are preferably cured. In curing of a liquid crystalline monomer, for example, after the liquid crystalline monomer is mixed with photopolymerization initiators, dispersed in a solution of a matrix component and oriented, in either of timing (before dyed or after dyed by iodine based light absorbing materials), the liquid crystalline monomer is cured by exposure with ultraviolet radiation etc. to stabilize orientation. Desirably, the liquid crystalline monomer is cured before dyed with iodine based light absorbing materials.

[0063]

As a process (4) in which the iodine based light absorbing material is dispersed in the translucent water-soluble resin used for forming the above-mentioned matrix, in general, a method in which the above-mentioned film is immersed into a bath of

aqueous system including iodine dissolved with auxiliary agents of iodide of alkali metals, such as potassium iodide may be mentioned. As mentioned above, an iodine based light absorbing material is formed by interaction between iodine dispersed in the matrix and the matrix resin. Timing of immersing may be before or after the above-mentioned stretching process (3). The iodine based light absorbing material is, in general, remarkably formed by being passed through a stretching process. A concentration of the aqueous system bath including iodine, and a proportion of the auxiliary agents, such as iodide of alkali metals may not especially be limited, but general iodine dyeing techniques may be adopted, and the above-mentioned concentration etc. may arbitrarily be changed.

[0064]

Moreover, a proportion of the iodine in the polarizer obtained is not especially limited, but a proportion of the translucent water-soluble resin and the iodine is preferably controlled to be 0.05 to 50 parts by weight grade to the translucent water-soluble resin 100 parts by weight, and more preferably 0.1 to 10 parts by weight.

[0065]

The process (5) in which the divalent metal is dispersing into a translucent water-soluble resin serving used for forming the above-mentioned matrix, in general, a method in which the above-mentioned film is immersed into an aqueous solution of a divalent metal. An iodide and the like of an alkaline metal such as potassium iodide may be dissolved into an aqueous solution of the divalent metal. The film may be immersed into the aqueous solution either before or after the stretching process (3) as a timing of the immersion. Moreover, a timing of the immersion may also

be either before or after the process (4) of dispersing an iodine light absorbing material.

[0066]

A proportion of the divalent metal ion relative to a translucent water-soluble resin both contained in an obtained polarizer is preferably controlled so as to be in the range of from 0.001 to 5 parts by weight, more preferably in the range of from 0.005 to 3 parts by weight and further more preferably in the range of from 0.01 to 1 parts by weight and especially preferably in the range of from 0.05 to 0.1 parts by weight relative to 100 parts by weight of the translucent water-soluble resin. If a proportion of the divalent metal ion relative to a translucent water-soluble resin is excessively large, a hue of the obtained polarizer is reddish, while a proportion of the divalent metal ion relative to a translucent water-soluble resin is excessively small, a hue of the obtained polarizer is bluish; therefore, neither of both cases is unpreferable because of possibility of an adverse influence on appearance. Accordingly, a concentration of a divalent metal aqueous solution is preferably in the range of from 0.01 to 10 weight %, more preferably in the range of from 0.05 to 5 weight % and further more preferably in the range of from 0.1 to 3 weight %. If a concentration of the divalent metal aqueous solution is excessively high, a concentration of the divalent metal ion in the polarizer is too high, unpreferably resulting in a reddish hue, while if a concentration of the divalent metal aqueous solution is excessively low, a concentration of the divalent metal ion in the polarizer is too low, unpreferably resulting in a bluish hue. An iodide of an alkaline metal such as potassium iodide may be dissolved in a divalent metal aqueous solution and no specific limitation is imposed on a concentration of the iodide or a

proportion thereof relative to a divalent metal ion and the concentration and the proportion can be arbitrarily varied.

[0067]

In production of the polarizer, processes for various purposes (6) may be given other than the above-mentioned processes (1) to (5). As a process (6), for example, a process in which a film is immersed in water bath and swollen may be mentioned for the purpose of mainly improving iodine dyeing efficiency of the film. Besides, a process in which a film is immersed in a water bath including arbitrary additives dissolved therein may be mentioned. A process in which a film is immersed in an aqueous solution including additives, such as boric acid and borax, for the purpose of cross-linking a water-soluble resin (matrix) may be mentioned. Moreover, for the purpose of mainly adjusting an amount balance of the dispersed iodine based light absorbing materials, and adjusting a hue, a process in which a film is immersed to an aqueous solution including additives, such as an iodide of an alkaline metals may be mentioned.

[0068]

As for the process (3) of orienting (stretching) of the above-mentioned film, the process (4) of dispersing and dyeing the iodine based light absorbing material into a matrix resin, the process (5) of immersing the divalent metal, and the above-mentioned process (6), so long as each of the processes (3), (4) and (5) is provided at least 1 time, respectively, a number, order and conditions (a bath temperature, immersion period of time, etc.) of the processes, may arbitrarily be selected, each process may separately be performed and furthermore a plurality of processes may simultaneously be performed. For example, a

cross-linking process of the process (6) and the stretching process (3) may be carried out simultaneously. A cross-linking process of the process (6) and the process (5) of immersing the divalent metal may be also carried out simultaneously.

5 [0069]

In addition, although the iodine based light absorbing material used for dyeing, the divalent metal, boric acid used for cross-linking are permeated into a film by immersing the film in an aqueous solution as mentioned above, instead of this method,
10 a method may be adopted that arbitrary types and amounts may be added before film formation of the process (2) and before or after preparation of a mixed solution in the process (1). And both methods may be used in combination. However, when high temperatures (for example, no less than 80°C) is required in the
15 process (3) at the time of stretching etc., in the view point of heat resistance of the iodine based light absorbing material, the process (4) for dispersing and dyeing the iodine based light absorbing material may be desirably performed after the process (3). And the process (5) of immersing the divalent metal may be
20 desirably performed after the process (4) for dispersing and dyeing the iodine based light absorbing material.

[0070]

A film given the above treatments is desirably dried using suitable conditions. Drying is performed according to
25 conventional methods.

[0071]

A thickness of the obtained polarizer (film) is not especially limited, in general, but it is 1 μm to 3 mm, preferably 5 μm to 1 mm, and more preferably 10 to 500 μm .

30 [0072]

A polarizer obtained in this way does not especially have a relationship in size between a refractive index of the birefringent material forming minute domains and a refractive index of the matrix resin in a stretching direction, whose stretching direction is in a Δn^1 direction and two directions perpendicular to a stretching axis are Δn^2 directions. Moreover, the stretching direction of an iodine based light absorbing material is in a direction demonstrating maximal absorption, and thus a polarizer having a maximally demonstrated effect of absorption and scattering may be realized.

[0073]

Since a polarizer obtained by this invention has equivalent functions as in existing absorbed type polarizing plates, it may be used in various applicable fields where absorbed type polarizing plates are used without any change.

[0074]

The above-described polarizer may be used as a polarizing plate with a transparent protective layer prepared at least on one side thereof using a usual method. The transparent protective layer may be prepared as an application layer by polymers, or a laminated layer of films. Proper transparent materials may be used as a transparent polymer or a film material that forms the transparent protective layer, and the material having outstanding transparency, mechanical strength, heat stability and outstanding moisture interception property, etc. may be preferably used. As materials of the above-mentioned protective layer, for example, polyester type polymers, such as polyethylene terephthalate and polyethylenenaphthalate; cellulose type polymers, such as diacetyl cellulose and triacetyl cellulose; acrylics type polymer, such as poly methylmethacrylate; styrene type polymers, such as

polystyrene and acrylonitrile-styrene copolymer (AS resin); polycarbonate type polymer may be mentioned. Besides, as examples of the polymer forming a protective film, polyolefin type polymers, such as polyethylene, polypropylene, polyolefin that has cyclo- type or norbornene structure, ethylene-propylene copolymer; vinyl chloride type polymer; amide type polymers, such as nylon and aromatic polyamide; imide type polymers; sulfone type polymers; polyether sulfone type polymers; polyether-ether ketone type polymers; poly phenylene sulfide type polymers; vinyl alcohol type polymer; vinylidene chloride type polymers; vinyl butyral type polymers; arylate type polymers; polyoxymethylene type polymers; epoxy type polymers; or blend polymers of the above-mentioned polymers may be mentioned. Films made of heat curing type or ultraviolet ray curing type resins, such as acryl based, urethane based, acryl urethane based, epoxy based, and silicone based, etc. may be mentioned.

[0075]

Moreover, as is described in Japanese Patent Laid-Open Publication No. 2001-343529 (WO 01/37007), polymer films, for example, resin compositions including (A) thermoplastic resins having substituted and/or non-substituted imido group in side chain, and (B) thermoplastic resins having substituted and/or non-substituted phenyl and nitrile group in sidechain may be mentioned. As an illustrative example, a film may be mentioned that is made of a resin composition including alternating copolymer comprising iso-butylene and N-methyl maleimide, and acrylonitrile-styrene copolymer. A film comprising mixture extruded article of resin compositions etc. may be used.

[0076]

As a transparent protection film, if polarization property and durability are taken into consideration, cellulose based polymer, such as triacetyl cellulose, is preferable, and especially triacetyl cellulose film is suitable. In general, a thickness of a transparent protection film is 500 μm or less, preferably 1 to 300 μm , and especially preferably 5 to 300 μm . In addition, when transparent protection films are provided on both sides of the polarizer, transparent protection films comprising same polymer material may be used on both of a front side and a back side, and transparent protection films comprising different polymer materials etc. may be used.

[0077]

Moreover, it is preferable that the transparent protection film may have as little coloring as possible. Accordingly, a protection film having a retardation value in a film thickness direction represented by $R_{th} = [(n_x + n_y) / 2 - n_z] \times d$ of -90 nm to +75 nm (where, n_x and n_y represent principal indices of refraction in a film plane, n_z represents refractive index in a film thickness direction, and d represents a film thickness) may be preferably used. Thus, coloring (optical coloring) of polarizing plate resulting from a protection film may mostly be cancelled using a protection film having a retardation value (R_{th}) of -90 nm to +75 nm in a thickness direction. The retardation value (R_{th}) in a thickness direction is preferably -80 nm to +60 nm, and especially preferably -70 nm to +45 nm.

[0078]

A hard coat layer may be prepared, or antireflection processing, processing aiming at sticking prevention, diffusion or anti glare may be performed onto the face on which the polarizing film of the above described transparent protective film has not

been adhered.

[0079]

A hard coat processing is applied for the purpose of protecting the surface of the polarizing plate from damage, and this hard coat film may be formed by a method in which, for example, a curable coated film with excellent hardness, slide property etc. is added on the surface of the protective film using suitable ultraviolet curable type resins, such as acrylic type and silicone type resins. Antireflection processing is applied for the purpose of antireflection of outdoor daylight on the surface of a polarizing plate and it may be prepared by forming an antireflection film according to the conventional method etc. Besides, a sticking prevention processing is applied for the purpose of adherence prevention with adjoining layer.

[0080]

In addition, an anti glare processing is applied in order to prevent a disadvantage that outdoor daylight reflects on the surface of a polarizing plate to disturb visual recognition of transmitting light through the polarizing plate, and the processing may be applied, for example, by giving a fine concavo-convex structure to a surface of the protective film using, for example, a suitable method, such as rough surfacing treatment method by sandblasting or embossing and a method of combining transparent fine particle. As a fine particle combined in order to form a fine concavo-convex structure on the above-mentioned surface, transparent fine particles whose average particle size is 0.5 to 50 μm , for example, such as inorganic type fine particles that may have conductivity comprising silica, alumina, titania, zirconia, tin oxides, indium oxides, cadmium oxides, antimony oxides, etc., and organic type

fine particles comprising cross-linked of non-cross-linked polymers may be used. When forming fine concavo-convex structure on the surface, the amount of fine particle used is usually about 2 to 50 weight parts to the transparent resin 100 weight parts that forms the fine concavo-convex structure on the surface, and preferably 5 to 25 weight parts. An anti glare layer may serve as a diffusion layer (viewing angle expanding function etc.) for diffusing transmitting light through the polarizing plate and expanding a viewing angle etc.

10 [0081]

In addition, the above-mentioned antireflection layer, sticking prevention layer, diffusion layer, anti glare layer, etc. may be built in the protective film itself, and also they may be prepared as an optical layer different from the protective layer.

15 [0082]

Adhesives are used for adhesion processing of the above described polarizing film and the transparent protective film. As adhesives, isocyanate derived adhesives, polyvinyl alcohol derived adhesives, gelatin derived adhesives, vinyl polymers derived latex type, aqueous polyesters derived adhesives, etc. may be mentioned. The above-described adhesives are usually used as adhesives comprising aqueous solution, and usually contain solid of 0.5 to 60 % by weight.

[0083]

25 A polarizing plate of the present invention is manufactured by adhering the above described transparent protective film and the polarizing film using the above described adhesives. The application of adhesives may be performed to any of the transparent protective film or the polarizing film, and may be performed to both of them. After adhered, drying process is given

30

and the adhesion layer comprising applied dry layer is formed.

Adhering process of the polarizing film and the transparent protective film may be performed using a roll laminator etc.

Although a thickness of the adhesion layer is not especially limited,
5 it is usually approximately 0.1 to 5 μm .

[0084]

A polarizing plate of the present invention may be used in practical use as an optical film laminated with other optical layers.

Although there is especially no limitation about the optical layers,

10 one layer or two layers or more of optical layers, which may be used for formation of a liquid crystal display etc., such as a

reflector, a transfective plate, a retardation plate (a half wavelength plate and a quarter wavelength plate included), and a

viewing angle compensation film, may be used. Especially

15 preferable polarizing plates are; a reflection type polarizing plate or a transfective type polarizing plate in which a reflector or a

transfective reflector is further laminated onto a polarizing plate of the present invention; an elliptically polarizing plate or a

circular polarizing plate in which a retardation plate is further

20 laminated onto the polarizing plate; a wide viewing angle polarizing plate in which a viewing angle compensation film is further

laminated onto the polarizing plate; or a polarizing plate in which a brightness enhancement film is further laminated onto the

polarizing plate.

25 [0085]

A reflective layer is prepared on a polarizing plate to give a reflection type polarizing plate, and this type of plate is used for

a liquid crystal display in which an incident light from a view side (display side) is reflected to give a display. This type of

30 plate does not require built-in light sources, such as a backlight,

but has an advantage that a liquid crystal display may easily be made thinner. A reflection type polarizing plate may be formed using suitable methods, such as a method in which a reflective layer of metal etc. is, if required, attached to one side of a polarizing plate through a transparent protective layer etc. [0086]

As an example of a reflection type polarizing plate, a plate may be mentioned on which, if required, a reflective layer is formed using a method of attaching a foil and vapor deposition film of reflective metals, such as aluminum, to one side of a matte treated protective film. Moreover, a different type of plate with a fine concavo-convex structure on the surface obtained by mixing fine particle into the above-mentioned protective film, on which a reflective layer of concavo-convex structure is prepared, may be mentioned. The reflective layer that has the above-mentioned fine concavo-convex structure diffuses incident light by random reflection to prevent directivity and glaring appearance, and has an advantage of controlling unevenness of light and darkness etc. Moreover, the protective film containing the fine particle has an advantage that unevenness of light and darkness may be controlled more effectively, as a result that an incident light and its reflected light that is transmitted through the film are diffused. A reflective layer with fine concavo-convex structure on the surface effected by a surface fine concavo-convex structure of a protective film may be formed by a method of attaching a metal to the surface of a transparent protective layer directly using, for example, suitable methods of a vacuum evaporation method, such as a vacuum deposition method, an ion plating method, and a sputtering method, and a plating method etc.

[0087]

Instead of a method in which a reflection plate is directly given to the protective film of the above-mentioned polarizing plate, a reflection plate may also be used as a reflective sheet constituted by preparing a reflective layer on the suitable film for the transparent film. In addition, since a reflective layer is usually made of metal, it is desirable that the reflective side is covered with a protective film or a polarizing plate etc. when used, from a viewpoint of preventing deterioration in reflectance by oxidation, of maintaining an initial reflectance for a long period of time and of avoiding preparation of a protective layer separately etc.

[0088]

In addition, a transflective type polarizing plate may be obtained by preparing the above-mentioned reflective layer as a transflective type reflective layer, such as a half-mirror etc. that reflects and transmits light. A transflective type polarizing plate is usually prepared in the backside of a liquid crystal cell and it may form a liquid crystal display unit of a type in which a picture is displayed by an incident light reflected from a view side (display side) when used in a comparatively well-lighted atmosphere. And this unit displays a picture, in a comparatively dark atmosphere, using embedded type light sources, such as a back light built in backside of a transflective type polarizing plate. That is, the transflective type polarizing plate is useful to obtain of a liquid crystal display of the type that saves energy of light sources, such as a back light, in a well-lighted atmosphere, and can be used with a built-in light source if needed in a comparatively dark atmosphere etc.

[0089]

The above-mentioned polarizing plate may be used as elliptically polarizing plate or circularly polarizing plate on which the retardation plate is laminated. A description of the above-mentioned elliptically polarizing plate or circularly polarizing plate will be made in the following paragraph. These polarizing plates change linearly polarized light into elliptically polarized light or circularly polarized light, elliptically polarized light or circularly polarized light into linearly polarized light or change the polarization direction of linearly polarization by a function of the retardation plate. As a retardation plate that changes circularly polarized light into linearly polarized light or linearly polarized light into circularly polarized light, what is called a quarter wavelength plate (also called $\lambda/4$ plate) is used. Usually, half-wavelength plate (also called $\lambda/2$ plate) is used, when changing the polarization direction of linearly polarized light.

[0090]

Elliptically polarizing plate is effectively used to give a monochrome display without above-mentioned coloring by compensating (preventing) coloring (blue or yellow color) produced by birefringence of a liquid crystal layer of a super twisted nematic (STN) type liquid crystal display. Furthermore, a polarizing plate in which three-dimensional refractive index is controlled may also preferably compensate (prevent) coloring produced when a screen of a liquid crystal display is viewed from an oblique direction. Circularly polarizing plate is effectively used, for example, when adjusting a color tone of a picture of a reflection type liquid crystal display that provides a colored picture, and it also has function of antireflection. For example, a retardation plate may be used that compensates coloring and

viewing angle, etc. caused by birefringence of various wavelength plates or liquid crystal layers etc. Besides, optical characteristics, such as retardation, may be controlled using laminated layer with two or more sorts of retardation plates having suitable retardation value according to each purpose. As retardation plates, birefringence films formed by stretching films comprising suitable polymers, such as polycarbonates, norbornene type resins, polyvinyl alcohols, polystyrenes, poly methyl methacrylates, polypropylene; polyarylates and polyamides; oriented films comprising liquid crystal materials, such as liquid crystal polymer; and films on which an alignment layer of a liquid crystal material is supported may be mentioned. A retardation plate may be a retardation plate that has a proper retardation according to the purposes of use, such as various kinds of wavelength plates and plates aiming at compensation of coloring by birefringence of a liquid crystal layer and of visual angle, etc., and may be a retardation plate in which two or more sorts of retardation plates is laminated so that optical properties, such as retardation, may be controlled.

[0091]

The above-mentioned elliptically polarizing plate and an above-mentioned reflected type elliptically polarizing plate are laminated plate combining suitably a polarizing plate or a reflection type polarizing plate with a retardation plate. This type of elliptically polarizing plate etc. may be manufactured by combining a polarizing plate (reflected type) and a retardation plate, and by laminating them one by one separately in the manufacture process of a liquid crystal display. On the other hand, the polarizing plate in which lamination was beforehand carried out and was obtained as an optical film, such as an

elliptically polarizing plate, is excellent in a stable quality, a workability in lamination etc., and has an advantage in improved manufacturing efficiency of a liquid crystal display.

[0092]

5 A viewing angle compensation film is a film for extending viewing angle so that a picture may look comparatively clearly, even when it is viewed from an oblique direction not from vertical direction to a screen. As such a viewing angle compensation retardation plate, in addition, a film having
10 birefringence property that is processed by uniaxial stretching or orthogonal bidirectional stretching and a bidirectionally stretched film as inclined orientation film etc. may be used. As inclined orientation film, for example, a film obtained using a method in which a heat shrinking film is adhered to a polymer
15 film, and then the combined film is heated and stretched or shrunk under a condition of being influenced by a shrinking force, or a film that is oriented in oblique direction may be mentioned. The viewing angle compensation film is suitably combined for the purpose of prevention of coloring caused by change of visible
20 angle based on retardation by liquid crystal cell etc. and of expansion of viewing angle with good visibility.

[0093]

 Besides, a compensation plate in which an optical anisotropy layer consisting of an alignment layer of liquid crystal
25 polymer, especially consisting of an inclined alignment layer of discotic liquid crystal polymer is supported with triacetyl cellulose film may preferably be used from a viewpoint of attaining a wide viewing angle with good visibility.

[0094]

30 The polarizing plate with which a polarizing plate and a

brightness enhancement film are adhered together is usually used being prepared in a backside of a liquid crystal cell. A brightness enhancement film shows a characteristic that reflects linearly polarized light with a predetermined polarization axis, or circularly polarized light with a predetermined direction, and that transmits other light, when natural light by back lights of a liquid crystal display or by reflection from a back-side etc., comes in. The polarizing plate, which is obtained by laminating a brightness enhancement film to a polarizing plate, thus does not transmit light without the predetermined polarization state and reflects it, while obtaining transmitted light with the predetermined polarization state by accepting a light from light sources, such as a backlight. This polarizing plate makes the light reflected by the brightness enhancement film further reversed through the reflective layer prepared in the backside and forces the light re-enter into the brightness enhancement film, and increases the quantity of the transmitted light through the brightness enhancement film by transmitting a part or all of the light as light with the predetermined polarization state. The polarizing plate simultaneously supplies polarized light that is difficult to be absorbed in a polarizer, and increases the quantity of the light usable for a liquid crystal picture display etc., and as a result luminosity may be improved. That is, in the case where the light enters through a polarizer from backside of a liquid crystal cell by the back light etc. without using a brightness enhancement film, most of the light, with a polarization direction different from the polarization axis of a polarizer, is absorbed by the polarizer, and does not transmit through the polarizer. This means that although influenced with the characteristics of the polarizer used, about 50 percent of light is

absorbed by the polarizer, the quantity of the light usable for a liquid crystal picture display etc. decreases so much, and a resulting picture displayed becomes dark. A brightness enhancement film does not enter the light with the polarizing direction absorbed by the polarizer into the polarizer but reflects the light once by the brightness enhancement film, and further makes the light reversed through the reflective layer etc. prepared in the backside to re-enter the light into the brightness enhancement film. By this above-mentioned repeated operation, only when the polarization direction of the light reflected and reversed between the both becomes to have the polarization direction which may pass a polarizer, the brightness enhancement film transmits the light to supply it to the polarizer. As a result, the light from a backlight may be efficiently used for the display of the picture of a liquid crystal display to obtain a bright screen.

[0095]

A diffusion plate may also be prepared between brightness enhancement film and the above described reflective layer, etc. A polarized light reflected by the brightness enhancement film goes to the above described reflective layer etc., and the diffusion plate installed diffuses passing light uniformly and changes the light state into depolarization at the same time. That is, the diffusion plate returns polarized light to natural light state. Steps are repeated where light, in the unpolarized state, i.e., natural light state, reflects through reflective layer and the like, and again goes into brightness enhancement film through diffusion plate toward reflective layer and the like. Diffusion plate that returns polarized light to the natural light state is installed between brightness enhancement film and the above described reflective layer, and the

like, in this way, and thus a uniform and bright screen may be provided while maintaining brightness of display screen, and simultaneously controlling non-uniformity of brightness of the display screen. By preparing such diffusion plate, it is considered that number of repetition times of reflection of a first incident light increases with sufficient degree to provide uniform and bright display screen conjointly with diffusion function of the diffusion plate.

[0096]

The suitable films are used as the above-mentioned brightness enhancement film. Namely, multilayer thin film of a dielectric substance; a laminated film that has the characteristics of transmitting a linearly polarized light with a predetermined polarizing axis, and of reflecting other light, such as the multilayer laminated film of the thin film having a different refractive-index anisotropy; an aligned film of cholesteric liquid-crystal polymer; a film that has the characteristics of reflecting a circularly polarized light with either left-handed or right-handed rotation and transmitting other light, such as a film on which the aligned cholesteric liquid crystal layer is supported may be mentioned.

[0097]

Therefore, in the brightness enhancement film of a type that transmits a linearly polarized light having the above-mentioned predetermined polarization axis, by arranging the polarization axis of the transmitted light and entering the light into a polarizing plate as it is, the absorption loss by the polarizing plate is controlled and the polarized light can be transmitted efficiently. On the other hand, in the brightness enhancement film of a type that transmits a circularly polarized

light as a cholesteric liquid-crystal layer, the light may be entered into a polarizer as it is, but it is desirable to enter the light into a polarizer after changing the circularly polarized light to a linearly polarized light through a retardation plate, taking control an absorption loss into consideration. In addition, a circularly polarized light is convertible into a linearly polarized light using a quarter wavelength plate as the retardation plate. [0098]

A retardation plate that works as a quarter wavelength plate in a wide wavelength ranges, such as a visible-light band, is obtained by a method in which a retardation layer working as a quarter wavelength plate to a pale color light with a wavelength of 550 nm is laminated with a retardation layer having other retardation characteristics, such as a retardation layer working as a half-wavelength plate. Therefore, the retardation plate located between a polarizing plate and a brightness enhancement film may consist of one or more retardation layers. [0099]

In addition, also in a cholesteric liquid-crystal layer, a layer reflecting a circularly polarized light in a wide wavelength ranges, such as a visible-light band, may be obtained by adopting a configuration structure in which two or more layers with different reflective wavelength are laminated together. Thus a transmitted circularly polarized light in a wide wavelength range may be obtained using this type of cholesteric liquid-crystal layer. [0100]

Moreover, the polarizing plate may consist of multi-layered film of laminated layers of a polarizing plate and two of more of optical layers as the above-mentioned separated

type polarizing plate. Therefore, a polarizing plate may be a reflection type elliptically polarizing plate or a semi-transmission type elliptically polarizing plate, etc. in which the above-mentioned reflection type polarizing plate or a transfective type polarizing plate is combined with above described retardation plate respectively.

[0101]

Although an optical film with the above described optical layer laminated to the polarizing plate may be formed by a method in which laminating is separately carried out sequentially in manufacturing process of a liquid crystal display etc., an optical film in a form of being laminated beforehand has an outstanding advantage that it has excellent stability in quality and assembly workability, etc., and thus manufacturing processes ability of a liquid crystal display etc. may be raised. Proper adhesion means, such as an adhesive layer, may be used for laminating. On the occasion of adhesion of the above described polarizing plate and other optical films, the optical axis may be set as a suitable configuration angle according to the target retardation characteristics etc.

[0102]

In the polarizing plate mentioned above and the optical film in which at least one layer of the polarizing plate is laminated, an adhesive layer may also be prepared for adhesion with other members, such as a liquid crystal cell etc. As pressure sensitive adhesive that forms adhesive layer is not especially limited, and, for example, acrylic type polymers; silicone type polymers; polyesters, polyurethanes, polyamides, polyethers; fluorine type and rubber type polymers may be suitably selected as a base polymer. Especially, a pressure sensitive adhesive such as

acrylics type pressure sensitive adhesives may be preferably used, which is excellent in optical transparency, showing adhesion characteristics with moderate wettability, cohesiveness and adhesive property and has outstanding weather resistance, heat resistance, etc.

[0103]

Moreover, an adhesive layer with low moisture absorption and excellent heat resistance is desirable. This is because those characteristics are required in order to prevent foaming and peeling-off phenomena by moisture absorption, in order to prevent decrease in optical characteristics and curvature of a liquid crystal cell caused by thermal expansion difference etc. and in order to manufacture a liquid crystal display excellent in durability with high quality.

[0104]

The adhesive layer may contain additives, for example, such as natural or synthetic resins, adhesive resins, glass fibers, glass beads, metal powder, fillers comprising other inorganic powder etc., pigments, colorants and antioxidants. Moreover, it may be an adhesive layer that contains fine particle and shows optical diffusion nature.

[0105]

Proper method may be carried out to attach an adhesive layer to one side or both sides of the optical film. As an example, about 10 to 40 weight % of the pressure sensitive adhesive solution in which a base polymer or its composition is dissolved or dispersed, for example, toluene or ethyl acetate or a mixed solvent of these two solvents is prepared. A method in which this solution is directly applied on a polarizing plate top or an optical film top using suitable developing methods, such as

flow method and coating method, or a method in which an adhesive layer is once formed on a separator, as mentioned above, and is then transferred on a polarizing plate or an optical film may be mentioned.

5 [0106]

An adhesive layer may also be prepared on one side or both sides of a polarizing plate or an optical film as a layer in which pressure sensitive adhesives with different composition or different kind etc. are laminated together. Moreover, when
10 adhesive layers are prepared on both sides, adhesive layers that have different compositions, different kinds or thickness, etc. may also be used on front side and backside of a polarizing plate or an optical film. Thickness of an adhesive layer may be suitably determined depending on a purpose of usage or adhesive
15 strength, etc., and generally is 1 to 500 μm , preferably 5 to 200 μm , and more preferably 10 to 100 μm .

[0107]

A temporary separator is attached to an exposed side of an adhesive layer to prevent contamination etc., until it is
20 practically used. Thereby, it can be prevented that foreign matter contacts adhesive layer in usual handling. As a separator, without taking the above-mentioned thickness conditions into consideration, for example, suitable conventional sheet materials that is coated, if necessary, with release agents, such as silicone
25 type, long chain alkyl type, fluorine type release agents, and molybdenum sulfide may be used. As a suitable sheet material, plastics films, rubber sheets, papers, cloths, no woven fabrics, nets, foamed sheets and metallic foils or laminated sheets thereof may be used.

30 [0108]

In addition, in the present invention, ultraviolet absorbing property may be given to the above-mentioned each layer, such as a polarizer for a polarizing plate, a transparent protective film and an optical film etc. and an adhesive layer, using a method of adding UV absorbents, such as salicylic acid ester type compounds, benzophenol type compounds, benzotriazol type compounds, cyano acrylate type compounds, and nickel complex salt type compounds.

[0109]

An optical film of the present invention may be preferably used for manufacturing various equipment, such as liquid crystal display, etc. Assembling of a liquid crystal display may be carried out according to conventional methods. That is, a liquid crystal display is generally manufactured by suitably assembling several parts such as a liquid crystal cell, optical films and, if necessity, lighting system, and by incorporating driving circuit. In the present invention, except that an optical film by the present invention is used, there is especially no limitation to use any conventional methods. Also any liquid crystal cell of arbitrary type, such as TN type, and STN type, π type may be used.

[0110]

Suitable liquid crystal displays, such as liquid crystal display with which the above-mentioned optical film has been located at one side or both sides of the liquid crystal cell, and with which a backlight or a reflector is used for a lighting system may be manufactured. In this case, the optical film by the present invention may be installed in one side or both sides of the liquid crystal cell. When installing the optical films in both sides, they may be of the same type or of different type.

Furthermore, in assembling a liquid crystal display, suitable parts, such as diffusion plate, anti-glare layer, antireflection film, protective plate, prism array, lens array sheet, optical diffusion plate, and backlight, may be installed in suitable position in one layer or two or more layers.

[0111]

Subsequently, organic electro luminescence equipment (organic EL display) will be explained. Generally, in organic EL display, a transparent electrode, an organic luminescence layer and a metal electrode are laminated on a transparent substrate in an order configuring an illuminant (organic electro luminescence illuminant). Here, an organic luminescence layer is a laminated material of various organic thin films, and much compositions with various combination are known, for example, a laminated material of hole injection layer comprising triphenylamine derivatives etc., a luminescence layer comprising fluorescent organic solids, such as anthracene; a laminated material of electronic injection layer comprising such a luminescence layer and perylene derivatives, etc.; laminated material of these hole injection layers, luminescence layer, and electronic injection layer etc.

[0112]

An organic EL display emits light based on a principle that positive hole and electron are injected into an organic luminescence layer by impressing voltage between a transparent electrode and a metal electrode, the energy produced by recombination of these positive holes and electrons excites fluorescent substance, and subsequently light is emitted when excited fluorescent substance returns to ground state. A mechanism called recombination which takes place in a

intermediate process is the same as a mechanism in common diodes, and, as is expected, there is a strong non-linear relationship between electric current and luminescence strength accompanied by rectification nature to applied voltage.

5 [0113]

In an organic EL display, in order to take out luminescence in an organic luminescence layer, at least one electrode must be transparent. The transparent electrode usually formed with transparent electric conductor, such as
10 indium tin oxide (ITO), is used as an anode. On the other hand, in order to make electronic injection easier and to increase luminescence efficiency, it is important that a substance with small work function is used for cathode, and metal electrodes, such as Mg-Ag and Al-Li, are usually used.

15 [0114]

In organic EL display of such a configuration, an organic luminescence layer is formed by a very thin film about 10nm in thickness. For this reason, light is transmitted nearly completely through organic luminescence layer as through
20 transparent electrode. Consequently, since the light that enters, when light is not emitted, as incident light from a surface of a transparent substrate and is transmitted through a transparent electrode and an organic luminescence layer and then is reflected by a metal electrode, appears in front surface side of
25 the transparent substrate again, a display side of the organic EL display looks like mirror if viewed from outside.

[0115]

In an organic EL display containing an organic electro luminescence illuminant equipped with a transparent electrode
30 on a surface side of an organic luminescence layer that emits

light by impression of voltage, and at the same time equipped with a metal electrode on a back side of organic luminescence layer, a retardation plate may be installed between these transparent electrodes and a polarizing plate, while preparing the polarizing plate on the surface side of the transparent electrode.
[0116]

Since the retardation plate and the polarizing plate have function polarizing the light that has entered as incident light from outside and has been reflected by the metal electrode, they have an effect of making the mirror surface of metal electrode not visible from outside by the polarization action. If a retardation plate is configured with a quarter wavelength plate and the angle between the two polarization directions of the polarizing plate and the retardation plate is adjusted to $\pi/4$, the mirror surface of the metal electrode may be completely covered.
[0117]

This means that only linearly polarized light component of the external light that enters as incident light into this organic EL display is transmitted with the work of polarizing plate. This linearly polarized light generally gives an elliptically polarized light by the retardation plate, and especially the retardation plate is a quarter wavelength plate, and moreover when the angle between the two polarization directions of the polarizing plate and the retardation plate is adjusted to $\pi/4$, it gives a circularly polarized light.

[0118]

This circularly polarized light is transmitted through the transparent substrate, the transparent electrode and the organic thin film, and is reflected by the metal electrode, and then is transmitted through the organic thin film, the transparent

electrode and the transparent substrate again, and is turned into a linearly polarized light again with the retardation plate. And since this linearly polarized light lies at right angles to the polarization direction of the polarizing plate, it cannot be transmitted through the polarizing plate. As the result, mirror surface of the metal electrode may be completely covered.

Examples

[0119]

Examples of this invention will, hereinafter, be shown, and specific descriptions will be provided. In addition, "parts" in following sections represents parts by weight.

[0120]

Example 1

(Polarizer)

A polyvinyl alcohol aqueous solution with a solid matter content of 13 weight % in which a polyvinyl alcohol resin with a polymerization degree of 2400 and a saponification degree of 98.5 %, a liquid crystalline monomer (a nematic liquid crystal temperature is in the range of from 40 to 70°) having an acryloyl group at each of both terminals of a mesogen group and glycerin were mixed together so that a ratio of polyvinyl alcohol: a liquid crystalline monomer: glycerin = 100: 3: 15 (in weight ratio) and the mixture was heated to a temperature equal to or higher than a liquid crystal temperature range and agitated with a homomixer to thereby obtain a mixed solution. Bubbles existing in the mixed solution were defoamed by leaving the solution at room temperature (23°C) as it was, thereafter, the solution is coated by means of a casting method, subsequently thereto, and the wet coat

was dried and to thereafter obtains a whitened mixed film with a thickness of 70 μm . The mixed film was heat-treated at 130°C for 10 min.

[0121]

5 The mixed film was wet-stretched by performing the following steps: (i) a step of immersing the mixed film in a water bath at 30°C to be swollen, followed by stretching three times, (ii) a step of dyeing by immersing the stretched film in an aqueous solution (a concentration of 0.32 weight %) with a ratio of iodine: potassium iodide = 1:7 (in weight ratio) at 30°C, (iii) a step of crosslinking the film by immersing it in an 3 weight % aqueous solution of boric acid at 30°C, (iv) a step of immersing the film in a 3.5 weight % aqueous solution of boric acid at 55°C, followed by stretching two times (six times in total) and (v) a step of immersing the film in an aqueous solution containing 4 weight % of potassium iodide and 3 weight % zinc sulfate heptahydrate at 30°C. The wet stretched film, subsequently thereto, was dried at 50°C for 4 minutes to thereby obtain a polarizer.

[0122]

20 (Confirmation of Generation of Anisotropic Scattering and Measurement of Refractive Index)

25 The obtained polarizer was observed under a polarization microscope and it was able to be confirmed that numberless dispersed micro regions of a liquid crystalline monomer were formed in a polyvinyl alcohol matrix. The liquid crystalline monomer is oriented in a stretching direction and an average size of micro regions in the stretching direction (Δn^2 direction) was in the range of from 1 to 2 μm .

[0123]

30 Refractive indices of the matrix and the micro region were

separately measured. Measurement was conducted at 20°C. A refractive index of a stretched film constituted only of a polyvinyl alcohol film stretched in the same conditions as the wet stretching with the exception that an aqueous solution of the step (ii) was water itself (without dyeing) was measured with an Abbe's refractometer (measurement light wavelength with 589 nm) to obtain a refractive index in the stretching direction (Δn^1 direction) = 1.54 and a refractive index in Δn^2 direction = 1.52. Refractive indexes (n_e : an extraordinary light refractive index and n_o : an ordinary light refractive index) of a liquid crystalline monomer were measured. An ordinary light refractive index n_o was measured of the liquid crystalline monomer orientation-coated on a high refractive index glass which is vertical alignment-treated with an Abbe's refractometer (measurement light with 589 nm). On the other hand, the liquid crystalline monomer is injected into a liquid crystal cell which is homogenous alignment-treated and a retardation ($\Delta n \times d$) was measured with an automatic birefringence measurement instrument (automatic birefringence meter KOBRA21ADH) manufactured by Ohoji Keisokuki K.K.) and a cell gap (d) was measured separately with an optical interference method to calculate Δn from retardation/cell gap and to obtain the sum of Δn and n_o as n_e . An extraordinary light refractive index n_e (corresponding to a refractive index in the Δn^1 direction) = 1.66 and n_o (corresponding to a refractive index of Δn^2 direction) = 1.53. Therefore, calculation was resulted in $\Delta n^1 = 1.66 - 1.54 = 0.12$ and $\Delta n^2 = 1.52 - 1.52 = 0.00$. It was confirmed from the measurement described above that a desired anisotropic scattering was able to occur.

[0124]

Example 2

A polarizer was obtained in a similar way to that in Example 1 with the exception that in Example 1, 3 weight % of zinc sulfate heptahydrate in the step (v) was changed to 2 weight % of nickel chloride. The obtained polarizer was confirmed on generation of an anisotropic scattering and a refractive index, similar to those in Example 1.

[0125]

Example 3

A polarizer was obtained in a similar way to that in Example 1 with the exception that in Example 1, 3 weight % of potassium iodide and 1.5 weight % of zinc sulfate heptahydrate were added into the 3 weight % aqueous solution of boric acid in the step (iii). The obtained polarizer was confirmed on generation of an anisotropic scattering and a refractive index, similar to those in Example 1.

[0126]

Example 4

A polarizer was obtained in a similar way to that in Example 1 with the exception that in Example 1, 3 weight % of potassium iodide and 1.5 weight % of zinc sulfate heptahydrate were added into the 3 weight % aqueous solution of boric acid in the step (iii) and 3 weight % of potassium iodide and 1.5 weight % of zinc sulfate heptahydrate were added into the 3.5 weight % aqueous solution of boric acid in the step (iv). The obtained polarizer was confirmed on generation of an anisotropic scattering and a refractive index, similar to those in Example 1.

[0127]

Example 5

A polarizer was obtained in a similar way to that in Example 1 with the exception that in Example 1, 3 weight % of potassium

iodide and 1.5 weight % of zinc sulfate heptahydrate were added into the 3 weight % aqueous solution of boric acid in the step (iii), 3 weight % of potassium iodide and 1.5 weight % of zinc sulfate heptahydrate were added into the 3.5 weight % aqueous solution of boric acid in the step (iv) and the aqueous solution containing 4 weight % of potassium iodide and 3 weight % of zinc sulfate heptahydrate was changed to an aqueous solution containing a potassium iodide with a content of 2 weight % in the step (v). The obtained polarizer was confirmed on generation of an anisotropic scattering and a refractive index, similar to those in Example 1.

[0128]

Comparative Example 1

A polarizer was manufactured in a similar way to that in Example 1 with the exception that in Example 1, the liquid crystalline monomer was not used.

[0129]

Comparative Example 2

A polarizer was manufactured in a similar way to that in Example 2 with the exception that in Example 2, the liquid crystalline monomer was not used.

[0130]

Comparative Example 3

A polarizer was obtained in a similar way to that in Example 1 with the exception that in Example 1, the liquid crystalline monomer was not used and zinc sulfate heptahydrate was not added into the aqueous solution used in the step (v).

[0131]

Comparative Example 4

A polarizer was manufactured in a similar way to that in Example 5 with the exception that in Example 5, the liquid

crystalline monomer was not used.

[0132]

Comparative Example 5

5 A polarizer was manufactured in a similar way to that in
Example 5 with the exception that in Example 5, the liquid
crystalline monomer was not used and a quantity of addition of the
zinc sulfate heptahydrate added into an aqueous solution used in
the steps (iii) and (iv) was set to 20 weight % respectively.

[0133]

10 (Evaluation)

 A proportion (%) of a divalent metal ion was measured in the
polarizer obtained in each of the examples and the comparative
examples. Measurement was conducted with a fluorescence X-Ray
spectrometer (manufactured by Rigaku Corporation with a trade
15 name of ZSX) and contents (%) of zinc ions and nickel ions were
measured. Results of the measurement are shown in Table 1.

[0134]

 An adhesive made of a 7 weight % polyvinyl alcohol aqueous
solution was coated on both surfaces of the polarizers obtained in
20 the examples and the comparative examples and a triacetyl
cellulose film (a thickness of 80 μm) on an adhesion surface of
which was saponification-treated using a sodium hydroxide
aqueous solution was adhered to both surfaces of each of the
polarizers as a transparent protective film to thereby obtain a
25 polarizing plate.

[0135]

 Polarizers (sample) obtained in Examples and Comparative
examples were measured for optical properties using a
spectrophotometer with integrating sphere (manufactured by
30 Hitachi Ltd. U-4100). Transmittance to each linearly polarized

light was measured under conditions in which a completely polarized light obtained through Glan Thompson prism polarizer was set as 100%. Transmittance was calculated based on CIE 1931 standard colorimetric system, and is shown with Y value, for which relative spectral responsivity correction was carried out. Notation k_1 represents a transmittance of a linearly polarized light in a maximum transmittance direction, and k_2 represents a transmittance of a linearly polarized light perpendicular to the direction.

10 [0136]

A polarization degree P was calculated with an equation $P = \{(k_1 - k_2) / (k_1 + k_2)\} \times 100$. A transmittance T of a simple substance was calculated with an equation $T = (k_1 + k_2) / 2$.

[0137]

15 A change Δab in perpendicular hue when the absorption axes of two polarizing plates were in a perpendicular arrangement was obtained. A change Δab in perpendicular hue was a value obtained from an equation $\Delta ab = \sqrt{(a_{240} - a_0)^2 + (b_{240} - b_0)^2}$, wherein an initial perpendicular chromaticities are a_0 and b_0 and perpendicular chromaticities a_{240} and b_{240} when left for 240 hrs under condition of 80°C. An a value and a b value are a value a value and a b value in the Hunter's color system. Results are shown in Table 1.

20

[0138]

Table 1

	Proportion of divalent metal ion in polarizer (%)	Linearly polarized light transmittance (%)		Transmittance of simple substance (%)	Polarization degree (%)	Δab
		Maximum transmission direction (k_1)	Perpendicular direction (k_2)			
Example 1	0.017	86.9	0.03	43.5	99.93	1.2
Example 2	0.012	86.8	0.028	43.4	99.94	1.6
Example 3	0.061	86.8	0.029	43.4	99.93	1.2
Example 4	0.093	86.9	0.028	43.5	99.94	1.1
Example 5	0.088	86.9	0.028	43.5	99.94	1.0
Comparative Example 1	0.019	86.9	0.055	43.5	99.87	1.1
Comparative Example 2	0.016	86.8	0.05	43.4	99.88	1.4
Comparative Example 3	0	86.9	0.05	43.5	99.88	3.0
Comparative Example 4	0.090	86.8	0.053	43.4	99.88	1.1
Comparative Example 5	8.3	86.9	0.53	43.7	98.79	2.5

As shown in Table 1, the examples have the same level in transmittance of simple substance as the comparative examples, but the examples are improved in polarization degree as compared with the comparative examples. This shows that an effect of scattering anisotropy is added to an absorption dichroism of iodine to thereby improve a polarization performance. The Δab values of Examples 1, 2 and 4 and Comparative Examples 1, 2 and 4 are apparently smaller as compared with that of Comparative Example 3 containing no zinc and in a case of Example 5, a change in hue is extremely small. It is understood from such phenomena that the examples were good in thermal durability and a change in hue was suppressed. Besides, the comparative examples each with a larger content of zinc have larger Δab values, from which it is concluded that a content of zinc is in the range of the invention.

[0139]

As a polarizer having a similar structure as a structure of a polarizer of this invention, a polarizer in which a mixed phase of

a liquid crystalline birefringent material and an absorption dichroism material is dispersed in a resin matrix is disclosed in Japanese Patent Laid-Open No.2002-207118, whose effect is similar as that of this invention. However, as compared with a case where an absorption dichroism material exists in dispersed phase as in Japanese Patent Laid-Open No.2002-207118, since in a case where an absorption dichroism material exists in a matrix layer as in this invention a longer optical path length may be realized by which a scattered polarized light passes absorption layer, more scattered light may be absorbed. Therefore, this invention may demonstrate much higher effect of improvement in light polarizing performance. This invention may be realized with simple manufacturing process.

[0140]

Although an optical system to which a dichroic dye is added to either of continuous phase or dispersed phase is disclosed in Japanese Patent Laid-Open No.2000-506990, this invention has large special feature in a point of using not dichroic dye but iodine. The following advantages are realized when using not dichroic dye but iodine. (1) Absorption dichroism demonstrated with iodine is higher than by dichroic dye. Therefore, polarized light characteristics will also become higher if iodine is used for a polarizer obtained. (2) Iodine does not show absorption dichroism, before being added in a continuous phase (matrix phase), and after being dispersed in a matrix, an iodine based light absorbing material showing dichroism is formed by stretching. This point is different from a dichroic dye having dichroism before being added in a continuous phase. That is, iodine exists as iodine itself, when dispersed in a matrix. In this case, in general, iodine has a far

effective diffusibility in a matrix compared with a dichroic dye. As a result, iodine based light absorbing material is dispersed to all corners of a film more excellently than dichroic dye. Therefore, an effect of increasing optical path length by scattering anisotropy can be utilized for maximum, which increases polarized light function.

[0141]

A background of invention given in Japanese Patent Laid-Open No.2000-506990 describes that optical property of a stretched film in which liquid droplets of a liquid crystal are arranged in a polymer matrix is indicated by Aphonin et al. However, Aphonin et al. has mentioned an optical film comprising a matrix phase and a dispersed phase (liquid crystal component), without using a dichroic dye, and since a liquid crystal component is not a liquid crystal polymer or a polymerized liquid crystalline monomer, a liquid crystal component in the film concerned has a sensitive birefringence typically depending on temperatures. On the other hand, this invention provides a polarizer comprising a film having a structure where minute domains are dispersed in a matrix formed of a translucent water-soluble resin including an iodine based light absorbing material, furthermore, in a liquid crystalline material of this invention, in the case of a liquid crystal polymer, after it is orientated in a liquid crystal temperature range, cooled to room temperatures and thus orientation is fixed, in the case of a liquid crystalline monomer, similarly, after orientation, the orientation is fixed by ultraviolet curing etc., birefringence of minute domains formed by a liquid crystalline material does not change by the change of temperatures.

Industrial Applicability

[0142]

5 **A polarizer of the invention is high in polarization degree and good durability and can be used in a polarizing plate and an optical film. A polarizing plate and an optical film can be preferably employed in image displays such as a liquid crystal display, an organic EL display, CRT and PDP.**